

Coupling between circuit problems and eddy-current problems

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Maxwell equations

Maxwell equations can be written as:

$$\begin{cases} \epsilon \frac{\partial \mathcal{E}}{\partial t} - \text{curl } \mathcal{H} = -\sigma \mathcal{E} - \mathcal{J}_e & \text{(Maxwell–Ampère)} \\ \mu \frac{\partial \mathcal{H}}{\partial t} + \text{curl } \mathcal{E} = 0 & \text{(Faraday),} \end{cases}$$

where

- \mathcal{E} and \mathcal{H} are the electric and magnetic fields, respectively
- ϵ is the electric permittivity
- μ is the magnetic permeability
- σ is the conductivity
- \mathcal{J}_e is the applied current density.

Time-harmonic Maxwell equations

When interested in time-periodic phenomena, it is assumed that

$$\mathcal{J}_e(t, \mathbf{x}) = \operatorname{Re}[\mathbf{J}_e(\mathbf{x}) \exp(i\omega t)]$$

$$\mathcal{E}(t, \mathbf{x}) = \operatorname{Re}[\mathbf{E}(\mathbf{x}) \exp(i\omega t)]$$

$$\mathcal{H}(t, \mathbf{x}) = \operatorname{Re}[\mathbf{H}(\mathbf{x}) \exp(i\omega t)] ,$$

where $\omega \neq 0$ is the assigned frequency, and one obtains

$$\begin{cases} \operatorname{curl} \mathbf{H} - i\omega\epsilon\mathbf{E} - \boldsymbol{\sigma}\mathbf{E} = \mathbf{J}_e \\ \operatorname{curl} \mathbf{E} + i\omega\boldsymbol{\mu}\mathbf{H} = \mathbf{0} . \end{cases}$$

Time-harmonic eddy-current equations

If **the frequency is small** the displacement currents $\epsilon \frac{\partial \mathcal{E}}{\partial t}$ can be disregarded. Thus one finds the so-called **eddy-current** (or quasi-static) problem

$$\begin{cases} \operatorname{curl} \mathbf{H} - \sigma \mathbf{E} = \mathbf{J}_e & \text{in } \Omega \\ \operatorname{curl} \mathbf{E} + i\omega \mu \mathbf{H} = \mathbf{0} & \text{in } \Omega. \end{cases} \quad (1)$$

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Here Ω is a bounded domain in \mathbb{R}^3 , composed by two parts: Ω_C , a **conductor**, and Ω_I , its complementary part, an **insulator**, where the conductivity σ is vanishing.

We consider the case in which the geometry of Ω is simple (a “box”), while that of Ω_C can be of two different types: a cylinder that touches the boundary or an internal torus.

"Gauge" conditions

- Problem: in an insulator one has $\sigma = 0$, therefore \mathbf{E} is not uniquely determined in that region ($\mathbf{E} + \nabla\psi$ is still a solution).

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[Depending on the geometrical properties of Ω_I as well as on the boundary conditions on $\partial\Omega$, other "gauge" conditions for \mathbf{E} in Ω_I can be necessary: here we will not enter this aspect.]

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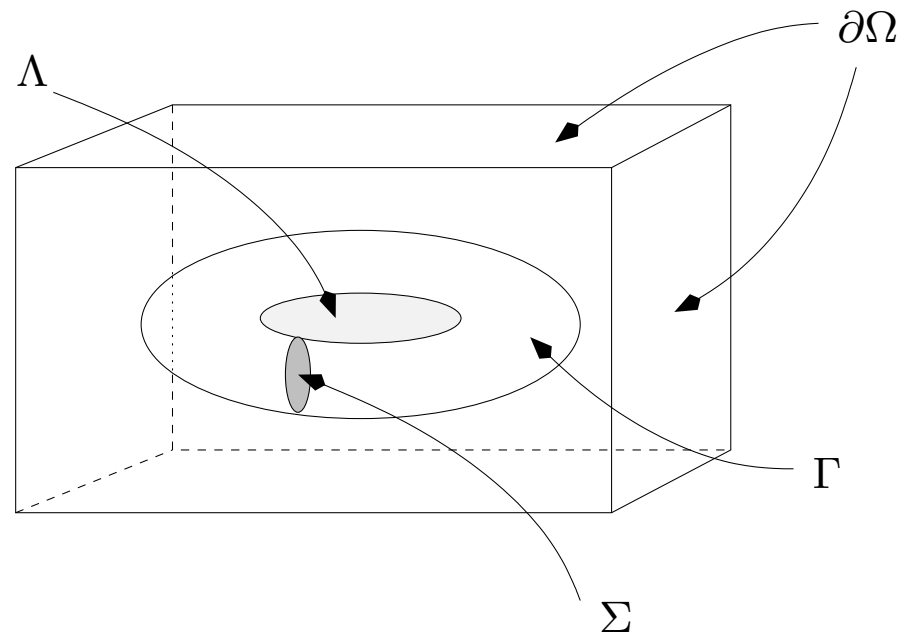
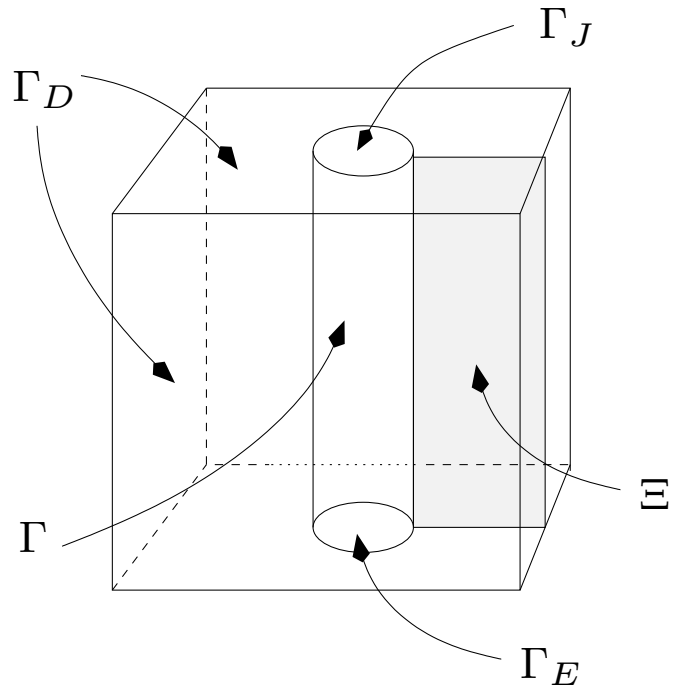
- **First geometrical case: electric ports.** The conductor Ω_C is not strictly contained in Ω . For simplicity, Ω_C is simply connected with $\partial\Omega_C \cap \partial\Omega = \Gamma_E \cup \Gamma_J$, where Γ_E and Γ_J are connected and disjoint surfaces on $\partial\Omega$ (“electric ports”). Notation: $\Gamma = \overline{\Omega_C} \cap \overline{\Omega_I}$, $\partial\Omega = \Gamma_E \cup \Gamma_J \cup \Gamma_D$, $\partial\Omega_C = \Gamma_E \cup \Gamma_J \cup \Gamma$, $\partial\Omega_I = \Gamma_D \cup \Gamma$.

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- **Second geometrical case: internal conductor.** The conductor Ω_C is strictly contained in Ω . For simplicity, Ω_C is a torus. Notation: $\partial\Omega_C = \Gamma$, $\partial\Omega_I = \partial\Omega \cup \Gamma$.

The geometrical configurations



Geometry and boundary conditions (cont'd)

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- **Mixed [Bossavit, 2000].** One imposes $\mathbf{E} \times \mathbf{n} = \mathbf{0}$ on $\Gamma_E \cup \Gamma_J$, $\mu\mathbf{H} \cdot \mathbf{n} = 0$ and $\epsilon\mathbf{E} \cdot \mathbf{n} = 0$ on Γ_D for the electric port case, while one requires $\mu\mathbf{H} \cdot \mathbf{n} = 0$ and $\epsilon\mathbf{E} \cdot \mathbf{n} = 0$ on $\partial\Omega$ for the internal conductor case.

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- **Case A.** Electric ports, $\mathbf{E} \times \mathbf{n} = \mathbf{0}$ on $\partial\Omega$
- **Case B.** Electric ports, $\mathbf{E} \times \mathbf{n} = \mathbf{0}$ on $\Gamma_E \cup \Gamma_J$, $\mathbf{H} \times \mathbf{n} = \mathbf{0}$ and $\epsilon\mathbf{E} \cdot \mathbf{n} = 0$ on Γ_D

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- **Case C.** Electric ports, $\mathbf{E} \times \mathbf{n} = \mathbf{0}$ on $\Gamma_E \cup \Gamma_J$, $\mu\mathbf{H} \cdot \mathbf{n} = 0$ and $\epsilon\mathbf{E} \cdot \mathbf{n} = 0$ on Γ_D

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- **Case E.** Internal conductor, $\mathbf{H} \times \mathbf{n} = \mathbf{0}$ and $\epsilon\mathbf{E} \cdot \mathbf{n} = 0$ on $\partial\Omega$
- **Case F.** Internal conductor, $\mu\mathbf{H} \cdot \mathbf{n} = 0$ and $\epsilon\mathbf{E} \cdot \mathbf{n} = 0$ on $\partial\Omega$.

Voltage and current intensity

When one wants to couple the eddy-current problem with a circuit problem, one has to consider, as the only external datum that determines the solution, a **voltage** V or a **current intensity** I_0 .

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Question:

- how can we formulate the eddy-current problems when the excitation is given by a voltage or by a current intensity?

This is a delicate point, as eddy-current problems, for the **five** cases A, B, D, E, F, have **a unique solution** already before a voltage or a current intensity is assigned!

Poynting Theorem (energy balance)

In fact one has:

Uniqueness theorem. In the cases A, B, D, E, F, for the solution of the eddy-current problem (1) the magnetic field \mathbf{H} in Ω and the electric field \mathbf{E}_C in Ω_C are uniquely determined. [Adding the "gauge" conditions, also the electric field \mathbf{E}_I in Ω_I is uniquely determined.]

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Proof. Multiply the Faraday equation by $\overline{\mathbf{H}}$, integrate in Ω and integrate by parts: it holds

$$\begin{aligned} 0 &= \int_{\Omega} \operatorname{curl} \mathbf{E} \cdot \overline{\mathbf{H}} + \int_{\Omega} i\omega\mu\mathbf{H} \cdot \overline{\mathbf{H}} \\ &= \int_{\Omega} \mathbf{E} \cdot \operatorname{curl} \overline{\mathbf{H}} + \int_{\Omega} i\omega\mu\mathbf{H} \cdot \overline{\mathbf{H}} + \int_{\partial\Omega} \mathbf{n} \times \mathbf{E} \cdot \overline{\mathbf{H}} . \end{aligned}$$

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Replacing \mathbf{E}_C with $\sigma^{-1}(\operatorname{curl} \mathbf{H}_C - \mathbf{J}_{e,C})$, and remembering that $\operatorname{curl} \mathbf{H}_I = \mathbf{J}_{e,I}$ in Ω_I , one has the **Poynting Theorem** (energy balance)

Poynting Theorem (energy balance) (cont'd)

$$\begin{aligned} & \int_{\Omega_C} \boldsymbol{\sigma}^{-1} \mathbf{J}_{e,C} \cdot \operatorname{curl} \overline{\mathbf{H}}_C - \int_{\Omega_I} \mathbf{E}_I \cdot \overline{\mathbf{J}}_{e,I} \\ &= \int_{\Omega_C} \boldsymbol{\sigma}^{-1} \operatorname{curl} \mathbf{H}_C \cdot \operatorname{curl} \overline{\mathbf{H}}_C + \int_{\Omega} i\omega \boldsymbol{\mu} \mathbf{H} \cdot \overline{\mathbf{H}} + \int_{\partial\Omega} \mathbf{n} \times \mathbf{E} \cdot \overline{\mathbf{H}}. \end{aligned}$$

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This is clearly vanishing in the cases **A**, **B**, **D** ed **E**.

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If $\mathbf{J}_e = 0$, we have only to take into account the term on $\partial\Omega$. This is clearly vanishing in the cases **A**, **B**, **D** ed **E**. In the case **F**, since $\operatorname{div}_\tau(\mathbf{E} \times \mathbf{n}) = -i\omega \boldsymbol{\mu} \mathbf{H} \cdot \mathbf{n} = 0$ on $\partial\Omega$, one has

$$\mathbf{E} \times \mathbf{n} = \operatorname{grad} W \times \mathbf{n} \text{ on } \partial\Omega ,$$

and therefore

$$\begin{aligned} \int_{\partial\Omega} \mathbf{n} \times \mathbf{E} \cdot \overline{\mathbf{H}} &= \int_{\partial\Omega} \overline{\mathbf{H}} \times \mathbf{n} \cdot \operatorname{grad} W = - \int_{\partial\Omega} \operatorname{div}(\overline{\mathbf{H}} \times \mathbf{n}) W \\ &= - \int_{\partial\Omega} \operatorname{curl} \overline{\mathbf{H}} \cdot \mathbf{n} W = 0 , \end{aligned}$$

as $\operatorname{curl} \mathbf{H}_I = 0$ in Ω_I and, for the case F, $\partial\Omega \subset \partial\Omega_I$. \square

Poynting Theorem for the case C

In the case **C**, instead, we can repeat the computation here above and find

$$\begin{aligned} \int_{\Omega_C} \boldsymbol{\sigma}^{-1} \operatorname{curl} \mathbf{H}_C \cdot \operatorname{curl} \overline{\mathbf{H}}_C + \int_{\Omega} i\omega \boldsymbol{\mu} \mathbf{H} \cdot \overline{\mathbf{H}} \\ = W_{|\Gamma_J} \int_{\Gamma_J} \operatorname{curl} \overline{\mathbf{H}}_C \cdot \mathbf{n} , \end{aligned}$$

where $W_{|\Gamma_J}$ is the (constant) value of the potential W on the electric port Γ_J (whereas $W_{|\Gamma_E} = 0$).

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where $W_{|\Gamma_J}$ is the (constant) value of the potential W on the electric port Γ_J (whereas $W_{|\Gamma_E} = 0$).

- In this case a degree of freedom is indeed still free (either the **voltage** $W_{|\Gamma_J}$, or else the **current intensity** $\int_{\Gamma_J} \operatorname{curl} \mathbf{H}_C \cdot \mathbf{n}$ in Ω_C).

The case C: variational formulation

- Thus we start from the case C: how can we formulate the problem when the source J_e and the voltage or the current intensity are assigned?
[Alonso Rodríguez, Valli and Vázquez Hernández, 2008; Bermúdez, Rodríguez and Salgado, 2005]

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This **orthogonal decomposition** result turns out to be useful: each vector function \mathbf{v}_I can be decomposed as

$$\mathbf{v}_I = \mu_I^{-1} \operatorname{curl} \mathbf{q}_I + \operatorname{grad} \psi_I + \alpha \boldsymbol{\rho}_I ,$$

where $\boldsymbol{\rho}_I$ is a harmonic field, namely, it belongs to the space

$$\mathcal{H}_{\mu_I}(\Omega_I) := \{ \mathbf{v}_I \in (L^2(\Omega_I))^3 \mid \operatorname{curl} \mathbf{v}_I = \mathbf{0}, \operatorname{div}(\boldsymbol{\mu}_I \mathbf{v}_I) = 0, \\ \boldsymbol{\mu}_I \mathbf{v}_I \cdot \mathbf{n} = 0 \text{ on } \partial\Omega_I \} .$$

The case C: variational formulation (cont'd)

The harmonic field ρ_I is **known** from the data of the problem, and satisfies $\int_{\partial\Gamma_J} \rho_I \cdot d\tau = 1$; moreover, from $\text{curl } \mathbf{v}_I = \mathbf{0}$ it follows $\mathbf{q}_I = \mathbf{0}$ and therefore $\alpha = \int_{\partial\Gamma_J} \mathbf{v}_I \cdot d\tau$.

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$$I_0 = \int_{\Gamma_J} \text{curl } \mathbf{H}_C \cdot \mathbf{n}_C = \int_{\partial\Gamma_J} \mathbf{H}_C \cdot d\tau = \int_{\partial\Gamma_J} \mathbf{H}_I \cdot d\tau = \alpha,$$

hence

$$\mathbf{H}_I = \text{grad } \psi_I + I_0 \rho_I. \quad (3)$$

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$$\mathbf{H}_I = \text{grad } \psi_I + I_0 \rho_I. \quad (3)$$

We want to provide a **"coupled"** variational formulation, in terms of \mathbf{E}_C in Ω_C and of \mathbf{H}_I in Ω_I .

The case C: variational formulation (cont'd)

Inserting the Faraday equation into the Ampère equation in Ω_C we find

$$\begin{aligned} \int_{\Omega_C} \mu_C^{-1} \mathbf{curl} \mathbf{E}_C \cdot \mathbf{curl} \overline{\mathbf{w}}_C + i\omega \int_{\Omega_C} \boldsymbol{\sigma} \mathbf{E}_C \cdot \overline{\mathbf{w}}_C \\ - i\omega \int_{\Gamma} \overline{\mathbf{w}}_C \times \mathbf{n}_C \cdot \mathbf{H}_I = -i\omega \int_{\Omega_C} \mathbf{J}_{e,C} \cdot \overline{\mathbf{w}}_C. \end{aligned} \quad (4)$$

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Instead, the Ampère equation in Ω_I gives

$$i\omega \int_{\Omega_I} \mu_I \mathbf{H}_I \cdot \operatorname{grad} \overline{\varphi}_I + \int_{\Gamma} \mathbf{E}_C \times \mathbf{n}_C \cdot \operatorname{grad} \overline{\varphi}_I = 0 \quad (5)$$

The case C: variational formulation (cont'd)

Inserting the Faraday equation into the Ampère equation in Ω_C we find

$$\int_{\Omega_C} \mu_C^{-1} \operatorname{curl} \mathbf{E}_C \cdot \operatorname{curl} \overline{\mathbf{w}}_C + i\omega \int_{\Omega_C} \boldsymbol{\sigma} \mathbf{E}_C \cdot \overline{\mathbf{w}}_C - i\omega \int_{\Gamma} \overline{\mathbf{w}}_C \times \mathbf{n}_C \cdot \mathbf{H}_I = -i\omega \int_{\Omega_C} \mathbf{J}_{e,C} \cdot \overline{\mathbf{w}}_C. \quad (4)$$

Instead, the Ampère equation in Ω_I gives

$$i\omega \int_{\Omega_I} \mu_I \mathbf{H}_I \cdot \operatorname{grad} \overline{\varphi}_I + \int_{\Gamma} \mathbf{E}_C \times \mathbf{n}_C \cdot \operatorname{grad} \overline{\varphi}_I = 0 \quad (5)$$

and

$$i\omega \int_{\Omega_I} \mu_I \mathbf{H}_I \cdot \boldsymbol{\rho}_I + \int_{\Gamma} \mathbf{E}_C \times \mathbf{n}_C \cdot \boldsymbol{\rho}_I = V. \quad (6)$$

The case C: variational formulation (cont'd)

Here we have to note that

$$\begin{aligned}\int_{\Gamma_D} \mathbf{E}_I \times \mathbf{n}_I \cdot \boldsymbol{\rho}_I &= \int_{\Gamma_D} \mathbf{grad} W \times \mathbf{n}_I \cdot \boldsymbol{\rho}_I \\ &= \int_{\Gamma_D} \operatorname{div}_\tau(\boldsymbol{\rho}_I \times \mathbf{n}_I) W + V \int_{\partial\Gamma_J} \boldsymbol{\rho}_I \cdot d\boldsymbol{\tau} = V .\end{aligned}$$

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Here we have to note that

$$\begin{aligned} \int_{\Gamma_D} \mathbf{E}_I \times \mathbf{n}_I \cdot \boldsymbol{\rho}_I &= \int_{\Gamma_D} \mathbf{grad} W \times \mathbf{n}_I \cdot \boldsymbol{\rho}_I \\ &= \int_{\Gamma_D} \operatorname{div}_\tau(\boldsymbol{\rho}_I \times \mathbf{n}_I) W + V \int_{\partial\Gamma_J} \boldsymbol{\rho}_I \cdot d\boldsymbol{\tau} = V . \end{aligned}$$

Using (3) in (4), (5) and (6) one has

$$\begin{aligned} &\int_{\Omega_C} \boldsymbol{\mu}_C^{-1} \operatorname{curl} \mathbf{E}_C \cdot \operatorname{curl} \overline{\mathbf{w}_C} + i\omega \int_{\Omega_C} \boldsymbol{\sigma} \mathbf{E}_C \cdot \overline{\mathbf{w}_C} \\ &\quad - i\omega \int_{\Gamma} \overline{\mathbf{w}_C} \times \mathbf{n}_C \cdot \mathbf{grad} \psi_I - i\omega I_0 \int_{\Gamma} \overline{\mathbf{w}_C} \times \mathbf{n}_C \cdot \boldsymbol{\rho}_I \quad (7) \\ &= -i\omega \int_{\Omega_C} \mathbf{J}_{e,C} \cdot \overline{\mathbf{w}_C} \end{aligned}$$

$$-i\omega \int_{\Gamma} \mathbf{E}_C \times \mathbf{n}_C \cdot \mathbf{grad} \overline{\varphi_I} + \omega^2 \int_{\Omega_I} \boldsymbol{\mu}_I \mathbf{grad} \psi_I \cdot \mathbf{grad} \overline{\varphi_I} = 0 \quad (8)$$

$$-i\omega \overline{Q} \int_{\Gamma} \mathbf{E}_C \times \mathbf{n}_C \cdot \boldsymbol{\rho}_I + \omega^2 I_0 \overline{Q} \int_{\Omega_I} \boldsymbol{\mu}_I \boldsymbol{\rho}_I \cdot \boldsymbol{\rho}_I = -i\omega V \overline{Q} . \quad (9)$$

The case C: existence and uniqueness

- If V is given, one solves (7), (8), (9) and determines \mathbf{E}_C , ψ_I and I_0 (hence \mathbf{H}_C and \mathbf{H}_I).

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Moreover, it is simple to propose an approximation method based on **finite elements**, of "edge" type for \mathbf{E}_C in Ω_C and of (scalar) nodal type for ψ_I in Ω_I . Convergence is assured by the Céa Lemma. [However, an efficient implementation demands to replace the harmonic field ρ_I with an easily computable function.]

The cases A, B, D, E, F

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The case C **comes back to help us**.

The cases A, B, D, E, F (cont'd)

In fact, let ϕ_C be the solution to

$$\left\{ \begin{array}{ll} \operatorname{div}(\boldsymbol{\sigma} \operatorname{grad} \phi_C) = 0 & \text{in } \Omega_C \\ \phi_C = 1 & \text{on } \Gamma_J \\ \phi_C = 0 & \text{on } \Gamma_E \\ \boldsymbol{\sigma} \operatorname{grad} \phi_C \cdot \mathbf{n} = 0 & \text{on } \Gamma . \end{array} \right.$$

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One easily verifies that $\mathbf{E}_C = V \operatorname{grad} \phi_C$ and $\mathbf{H} = \mathbf{0}$ is the solution to the problem C with $\mathbf{J}_{e,C} = -V \boldsymbol{\sigma} \operatorname{grad} \phi_C$ and assigned voltage V .

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$$\begin{aligned} \int_{\Omega_C} \boldsymbol{\sigma}^{-1} \mathbf{J}_{e,C} \cdot \operatorname{curl} \overline{\mathbf{H}_C} &= \int_{\Omega_C} (-V \operatorname{grad} \phi_C) \cdot \operatorname{curl} \overline{\mathbf{H}_C} \\ &= -V \int_{\Gamma \cup \Gamma_E \cup \Gamma_J} \phi_C \operatorname{curl} \overline{\mathbf{H}_C} \cdot \mathbf{n}_C \\ &= -V \int_{\Gamma_J} \operatorname{curl} \overline{\mathbf{H}_C} \cdot \mathbf{n}, \end{aligned}$$

The cases A, B, D, E, F (cont'd)

and from the Poynting Theorem

$$\begin{aligned} \int_{\Omega_C} \boldsymbol{\sigma}^{-1} \operatorname{curl} \mathbf{H}_C \cdot \operatorname{curl} \overline{\mathbf{H}}_C + \int_{\Omega} i\omega \boldsymbol{\mu} \mathbf{H} \cdot \overline{\mathbf{H}} \\ = V \int_{\Gamma_J} \operatorname{curl} \overline{\mathbf{H}}_C \cdot \mathbf{n} + \int_{\Omega_C} \boldsymbol{\sigma}^{-1} \mathbf{J}_{e,C} \cdot \operatorname{curl} \overline{\mathbf{H}}_C = 0, \end{aligned}$$

so that $\mathbf{H} = \mathbf{0}$, and, moreover, from the Ampère equation $\mathbf{E}_C = -\boldsymbol{\sigma}^{-1} \mathbf{J}_{e,C} = V \operatorname{grad} \phi_C$.

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Thus, by linearity, the magnetic field \mathbf{H} solution to problem (7), (8), (9) with data $\mathbf{J}_{e,C} = \mathbf{0}$ and $W|_{\Gamma_J} = V$ **is the same** than the one with data $\mathbf{J}_{e,C} = V \sigma \operatorname{grad} \phi_C$ and $W|_{\Gamma_J} = 0$.

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[Instead, for the electric field one has that the difference in Ω_C is given by $V \operatorname{grad} \phi_C$.]

The cases A, B, D, E, F (cont'd)

For the cases A, B (electric ports), for which the "electric" voltage cannot be assigned, one is thus led to consider a "source" voltage V , that is the factor appearing in the current density $\mathbf{J}_{e,C} = V \sigma \text{grad } \phi_C$, and to solve eddy-current problems with this source.

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Note that $\text{grad } \phi_C$ is the basis function of the space of harmonic fields

$$\hat{\mathcal{H}}(\Omega_C) := \{ \hat{\boldsymbol{\eta}}_C \in (L^2(\Omega_C))^3 \mid \text{curl } \hat{\boldsymbol{\eta}}_C = \mathbf{0}, \text{div}(\boldsymbol{\sigma} \hat{\boldsymbol{\eta}}_C) = 0, \\ \boldsymbol{\sigma} \hat{\boldsymbol{\eta}}_C \cdot \mathbf{n}_C = 0 \text{ on } \Gamma, \hat{\boldsymbol{\eta}}_C \times \mathbf{n} = \mathbf{0} \text{ on } \Gamma_E \cup \Gamma_J \} ,$$

normalized by the condition $\int_{\hat{\gamma}} \hat{\boldsymbol{\eta}}_C \cdot d\boldsymbol{\tau} = 1$, where $\hat{\gamma}$ is (any) path connecting Γ_E to Γ_J .

The cases A, B, D, E, F (cont'd)

Then, for the cases D, E, F (internal conductor) we define ρ_C the basis function of the space of harmonic fields

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normalized by the condition $\int_{\gamma} \boldsymbol{\rho}_C \cdot d\boldsymbol{\tau} = 1$, where the closed cycle γ runs internally along the whole torus Ω_C .

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Similarly to the cases A,B (electric ports), for the cases D, E, F (internal conductor) one can thus consider a "source" voltage V , associated with the current density $\mathbf{J}_{e,C} = V \boldsymbol{\sigma} \boldsymbol{\rho}_C$.

The voltage rule

- **The voltage rule.**

Having to impose a voltage V , **modify Ohm law in Ω_C** adding to the current density $\sigma \mathbf{E}_C$ the "applied" current density $\mathbf{J}_{e,C} = V \sigma \mathbf{Q}_C$, where $\mathbf{Q}_C = \text{grad } \phi_C$ for the electric port case, and $\mathbf{Q}_C = \rho_C$ for the internal conductor case. Thus Ampère law becomes

$$\text{curl } \mathbf{H}_C - \sigma \mathbf{E}_C = V \sigma \mathbf{Q}_C .$$

In the former case, we intend that the voltage passes from 0 on Γ_E to V on Γ_J ; in the latter case, the voltage passes from 0 to V along the internal cycle γ .

The current intensity rule

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Having to impose a current intensity I_0 , **modify Ohm law in Ω_C** adding to the current density $\sigma \mathbf{E}_C$ the "applied" current density $\mathbf{J}_{e,C} = V \sigma \mathbf{Q}_C$, where \mathbf{Q}_C is as in the "voltage rule" and V has to be determined. Thus the Ampère law reads

$$\mathbf{curl} \mathbf{H}_C - \sigma \mathbf{E}_C - V \sigma \mathbf{Q}_C = 0 .$$

Then determine the field quantities \mathbf{H} and \mathbf{E}_C and the voltage V in such a way that also the additional constraint

$$\int_S \mathbf{curl} \mathbf{H}_C \cdot \mathbf{n} = I_0$$

is satisfied.

The current intensity rule (cont'd)

In this constraint one has $S = \Gamma_J$ for the electric port case, and $S = \Sigma$, a section of Ω_C , for the internal conductor case. In the former case, the unit vector \mathbf{n} is the outward normal on Γ_J ; in the latter case, the unit vector \mathbf{n} on Σ has the same orientation of the internal cycle γ .

Caso F: variational formulation

As an example, let us give the variational formulation for the **case F**: given a voltage $V \neq 0$, the problem to solve is

$$\begin{aligned} \int_{\Omega_C} \sigma^{-1} \operatorname{curl} \mathbf{H}_C \cdot \operatorname{curl} \overline{\mathbf{w}_C} + \int_{\Omega} i\omega \mu \mathbf{H} \cdot \overline{\mathbf{w}} \\ = V \int_{\Omega_C} \rho_C \cdot \operatorname{curl} \overline{\mathbf{w}_C} \end{aligned} \quad (10)$$

for all $\mathbf{w} \in X$, where

$$X := \{ \mathbf{w} \in H(\operatorname{curl}; \Omega) \mid \operatorname{curl} \mathbf{w}_I = \mathbf{0} \text{ in } \Omega_I \} .$$

Then one computes $I_0 = \int_{\Omega_C} \rho_C \cdot \operatorname{curl} \mathbf{H}_C \neq 0$ [note that $\overline{I_0} = V^{-1} (\int_{\Omega_C} \sigma^{-1} \operatorname{curl} \mathbf{H}_C \cdot \operatorname{curl} \overline{\mathbf{H}_C} + \int_{\Omega} i\omega \mu \mathbf{H} \cdot \overline{\mathbf{H}}) \dots$] and defines $\mathbf{E}_C = \sigma^{-1} \operatorname{curl} \mathbf{H}_C - V \rho_C$.

Caso F: variational formulation (cont'd)

Instead, given the current intensity $I_0 \neq 0$, the problem is

$$\begin{cases} \int_{\Omega_C} \boldsymbol{\sigma}^{-1} \operatorname{curl} \mathbf{H}_C \cdot \operatorname{curl} \overline{\mathbf{w}}_C + \int_{\Omega} i\omega \boldsymbol{\mu} \mathbf{H} \cdot \overline{\mathbf{w}} \\ -V \int_{\Omega_C} \boldsymbol{\rho}_C \cdot \operatorname{curl} \overline{\mathbf{w}}_C = 0 \\ \int_{\Omega_C} \boldsymbol{\rho}_C \cdot \operatorname{curl} \mathbf{H}_C = I_0 \end{cases}$$

for all $\mathbf{w} \in X$, and the voltage $V \neq 0$ [note that

$V = \overline{I_0}^{-1} (\int_{\Omega_C} \boldsymbol{\sigma}^{-1} \operatorname{curl} \mathbf{H}_C \cdot \operatorname{curl} \overline{\mathbf{H}}_C + \int_{\Omega} i\omega \boldsymbol{\mu} \mathbf{H} \cdot \overline{\mathbf{H}}) \dots$] turns out to be a Lagrange multiplier associated with the constraint requiring that the intensity current is equal to I_0 .

Then, as usual, one defines $\mathbf{E}_C = \boldsymbol{\sigma}^{-1} \operatorname{curl} \mathbf{H}_C - V \boldsymbol{\rho}_C$.

Don't forget the Faraday law!

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Since

$$V \int_{\Omega_C} \rho_C \cdot \mathbf{curl} \overline{\mathbf{w}_C} = V \int_{\Gamma} \rho_C \times \mathbf{n}_C \cdot \overline{\mathbf{w}_C} ,$$

and this term is vanishing for a test function \mathbf{w}_C with a compact support in Ω_C , one verifies that **the Faraday equation in Ω_C** is satisfied, and, having set

$\mathbf{E}_C = \sigma^{-1} \mathbf{curl} \mathbf{H}_C$, the same clearly holds for the **Ampère equation (without sources) in the whole Ω** .

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[**Note**: since the electric field \mathbf{E}_I is determined by solving the Faraday equation in Ω_I (with \mathbf{H}_I already known), **one is led to believe** that everything is all right...]

Don't forget the Faraday law! (cont'd)

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Don't forget the Faraday law! (cont'd)

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Let us see: the Faraday law relates the flux of the magnetic induction through a surface with the line integral of the electric field on the boundary of that surface.

Since we know the magnetic field in the whole Ω , **surfaces can stay everywhere**; but at the moment we know the electric field only in Ω_C , therefore **the boundary of the surface must stay in $\overline{\Omega_C}$** .

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But the Faraday law (in differential form) is satisfied in Ω_C .

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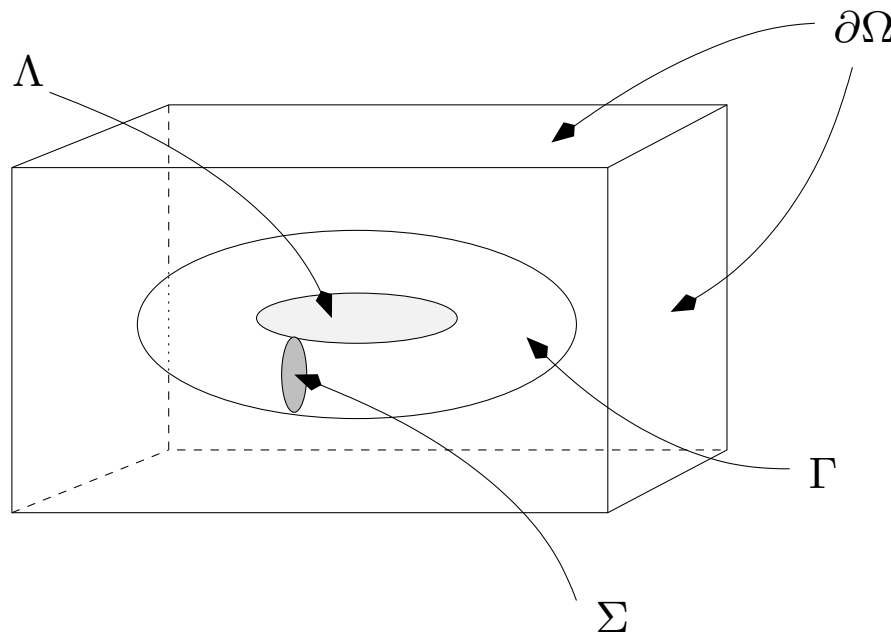
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But the Faraday law (in differential form) is satisfied in Ω_C . Thus we must verify if there are **surfaces in Ω_I with boundary on Γ** , and moreover such that this boundary **is not the boundary of a surface in Ω_C** [if this is not the case, the Divergence Theorem says that again everything is all right, as the magnetic induction is divergence free in $\Omega...$].

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- Claim: the Faraday law is violated **on the "cutting" surface Λ !**



Don't forget the Faraday law! (cont'd)

In fact, the Faraday law on Λ can be written as

$$\int_{\Omega_I} i\omega\mu_I \mathbf{H}_I \cdot \boldsymbol{\rho}_I + \int_{\Gamma} (\mathbf{E}_C \times \mathbf{n}_C) \cdot \boldsymbol{\rho}_I = 0 ,$$

and from (10) we have

$$\begin{aligned} \int_{\Omega_I} i\omega\mu_I \mathbf{H}_I \cdot \boldsymbol{\rho}_I &= - \int_{\Omega_C} i\omega\mu_C \mathbf{H}_C \cdot \mathbf{R}_C \\ &+ V \int_{\Omega_C} \boldsymbol{\rho}_C \cdot \mathbf{curl} \mathbf{R}_C - \int_{\Omega_C} \boldsymbol{\sigma}^{-1} \mathbf{curl} \mathbf{H}_C \cdot \mathbf{curl} \mathbf{R}_C , \end{aligned}$$

where \mathbf{R}_C is any (real) extension of $\boldsymbol{\rho}_I$ in Ω_C giving a global function that belongs to the space X .

Don't forget the Faraday law! (cont'd)

Setting $\mathbf{E}_C = \sigma^{-1} \operatorname{curl} \mathbf{H}_C$ and integrating by parts one has

$$\begin{aligned} V \int_{\Omega_C} \boldsymbol{\rho}_C \cdot \operatorname{curl} \mathbf{R}_C - \int_{\Omega_C} \mathbf{E}_C \cdot \operatorname{curl} \mathbf{R}_C &= V \int_{\Gamma} (\boldsymbol{\rho}_C \times \mathbf{n}_C) \cdot \boldsymbol{\rho}_I \\ &+ \int_{\Omega_C} i\omega \boldsymbol{\mu}_C \mathbf{H}_C \cdot \mathbf{R}_C - \int_{\Gamma} (\mathbf{E}_C \times \mathbf{n}_C) \cdot \boldsymbol{\rho}_I, \end{aligned}$$

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[**Note:** what is wrong in the previous argument? We cannot find the electric field \mathbf{E}_I such that $\operatorname{curl} \mathbf{E}_I = -i\omega \boldsymbol{\mu}_I \mathbf{H}_I$ in Ω_I and $\mathbf{E}_I \times \mathbf{n}_I = -\mathbf{E}_C \times \mathbf{n}_C$ on Γ : **a necessary compatibility condition on the data is not satisfied!**]

Cases A, B, D, E, F: existence and uniqueness

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- The problem with a given voltage is therefore a standard eddy-current problem, but with a particular assigned current density $J_{e,C}$, hence it has a unique solution.
- The problem with a given current intensity is instead a saddle-point problem, and it needs a deeper analysis. In conclusion, however, it turns out to have a unique solution, too.

Cases A, B, D, E, F: numerical approximation

- For the voltage problem one can use any numerical approximation method that is suitable for eddy-current problems. [For a more efficient implementation, it is better to replace the functions $\text{grad } \phi_C$ or ρ_C with a term that can be easily computed.]

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- For the current intensity problem, one has to use those numerical approximation methods that are suitable for saddle-point problems. [However, note that the current intensity constraint is associated with only one degree of freedom, therefore one is facing a rather simple extension of usual eddy-current problems.]

Numerical results for the Case C

Coming back to the case C and to its variational formulation (7), (8), (9), we use **edge finite elements of the lowest degree** ($\mathbf{a} + \mathbf{b} \times \mathbf{x}$ in each element) for approximating \mathbf{E}_C , and **scalar piecewise linear elements** for approximating ψ_I .

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The problem description is the following: the conductor Ω_C and the whole domain Ω are two coaxial cylinders of radius R_C and R_D , respectively, and height L . Assuming that σ and μ are scalar constants, the exact solution for an assigned current intensity I_0 is known (through suitable Bessel functions), and also the basis function ρ_I is known, thus from (9) one easily computes the voltage V , too.

Numerical results for the Case C (cont'd)

We have the following data:

$$R_C = 0.25 \text{ m}$$

$$R_D = 0.5 \text{ m}$$

$$L = 0.25 \text{ m}$$

$$\sigma = 151565.8 \text{ } \Omega^{-1} \text{ m}^{-1}$$

$$\mu = 4\pi \times 10^{-7} \text{ Hm}^{-1}$$

$$\omega = 50 \times 2\pi \text{ rad/s}$$

and

$$I_0 = 10^4 \text{ A} \quad \text{or} \quad V = 0.08979 + 0.14680i$$

[the voltage corresponds to the current intensity $I_0 = 10^4 \text{ A}$].

Numerical results for the Case C (cont'd)

The relative errors (for \mathbf{E}_C in $H(\text{curl}; \Omega_C)$ and for \mathbf{H}_I in $L^2(\Omega_I)$) with respect to the number of degrees of freedom are given by:

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Elements	DoF	e_E	e_H	e_V
2304	1684	0.2341	0.1693	0.0312
18432	11240	0.1132	0.0847	0.0089
62208	35580	0.0750	0.0567	0.0048
147456	81616	0.0561	0.0425	0.0018

Numerical results for the Case C (cont'd)

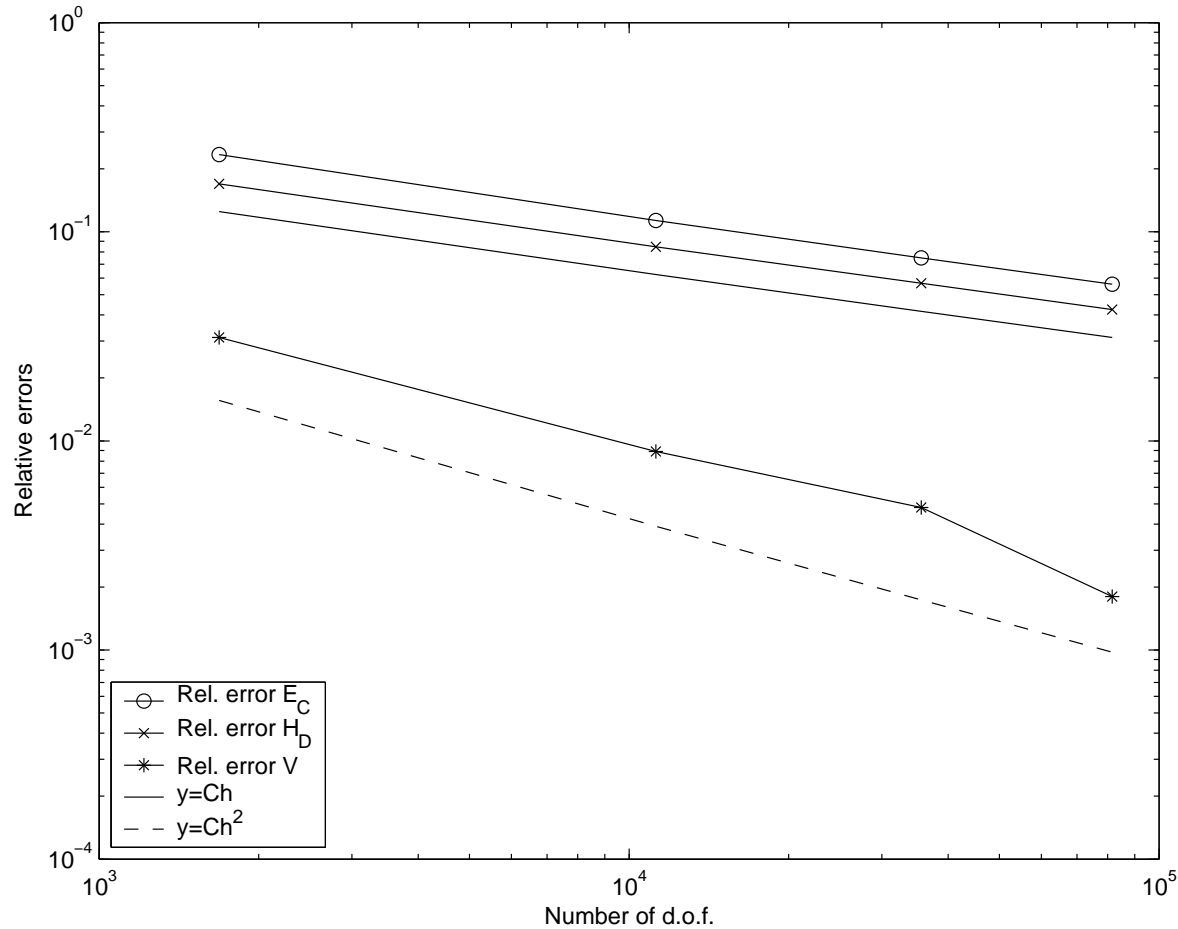
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Elements	DoF	e_E	e_H	e_I
2304	1685	0.2336	0.1685	0.0274
18432	11241	0.1132	0.0847	0.0085
62208	35581	0.0750	0.0566	0.0041
147456	81617	0.0561	0.0425	0.0024

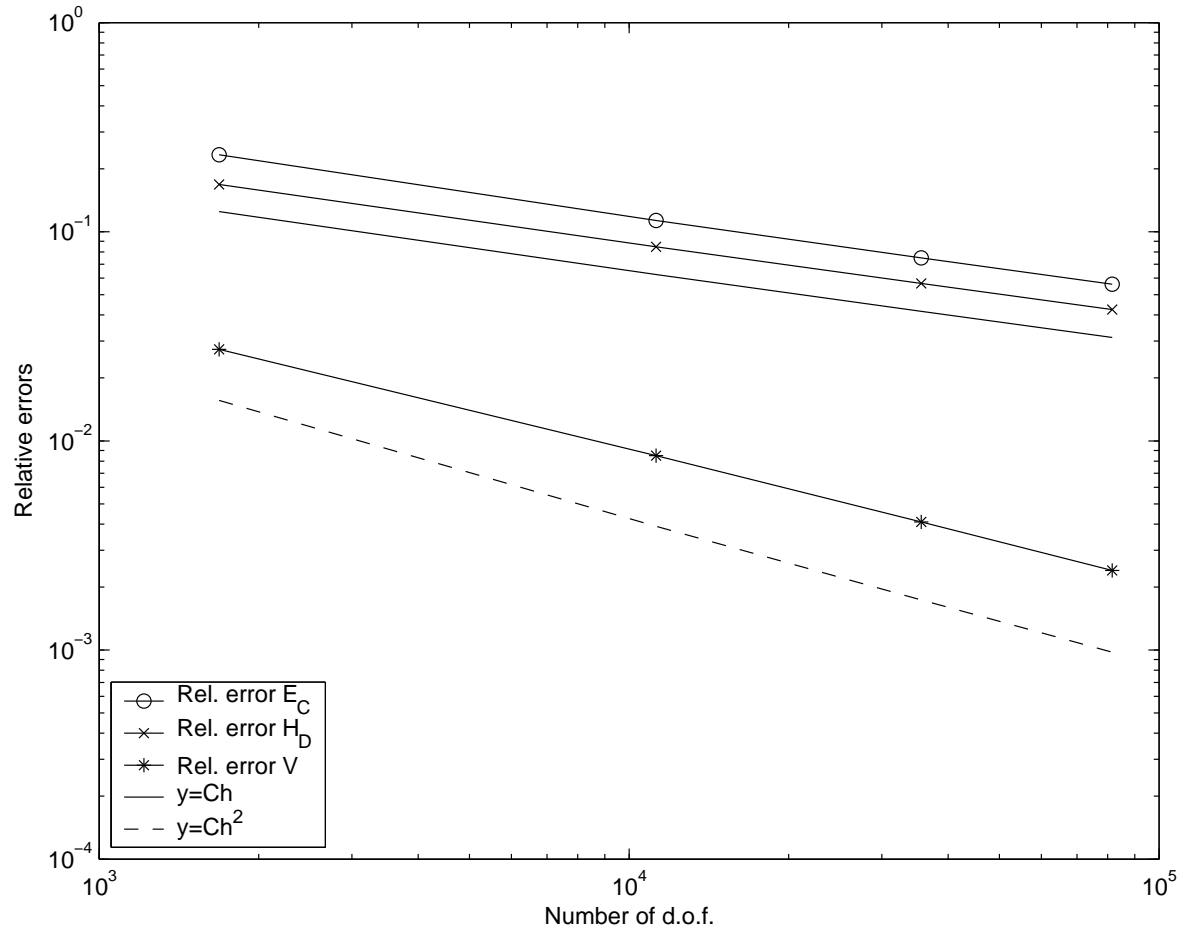
Numerical results for the Case C (cont'd)

On a graph: for assigned current intensity



Numerical results for the Case C (cont'd)

for assigned voltage



Numerical results for the Case C (cont'd)

A more realistic problem, considered by Bermúdez, Rodríguez and Salgado, 2005, is that of a cylindrical electric furnace with three electrodes ELSA [dimensions: furnace height 2 m.; furnace diameter 8.88 m.; electrode height 1.25 m.; electrode diameter 1 m.; distance of the center of the electrode from the wall 3 m.].

Numerical results for the Case C (cont'd)

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The three electrodes ELSA are constituted by a graphite core of 0.4 m. of diameter, and by an outer part of Söderberg paste. The electric current enters the electrodes through horizontal copper bars of rectangular section (0.07 m. \times 0.25 m.), connecting the top of the electrode with the external boundary.

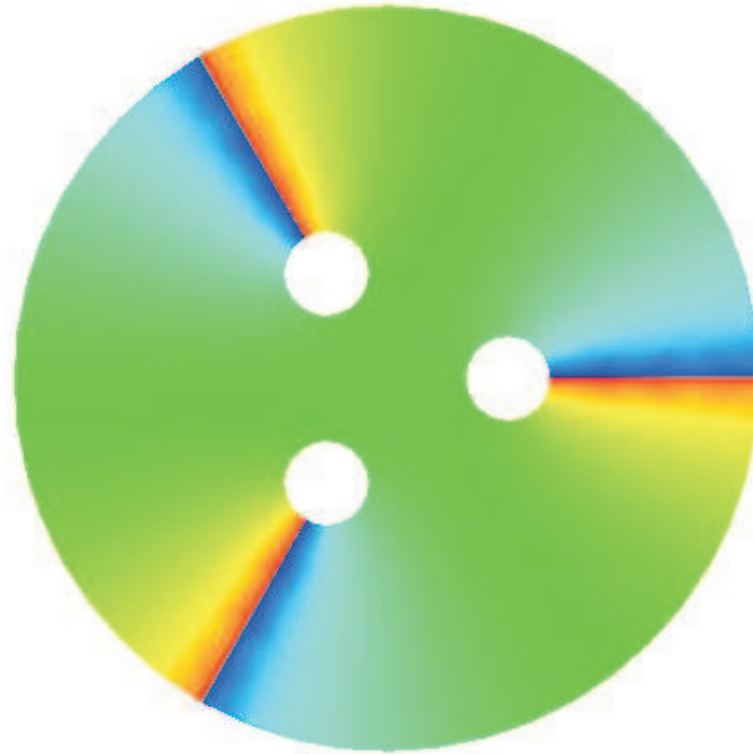
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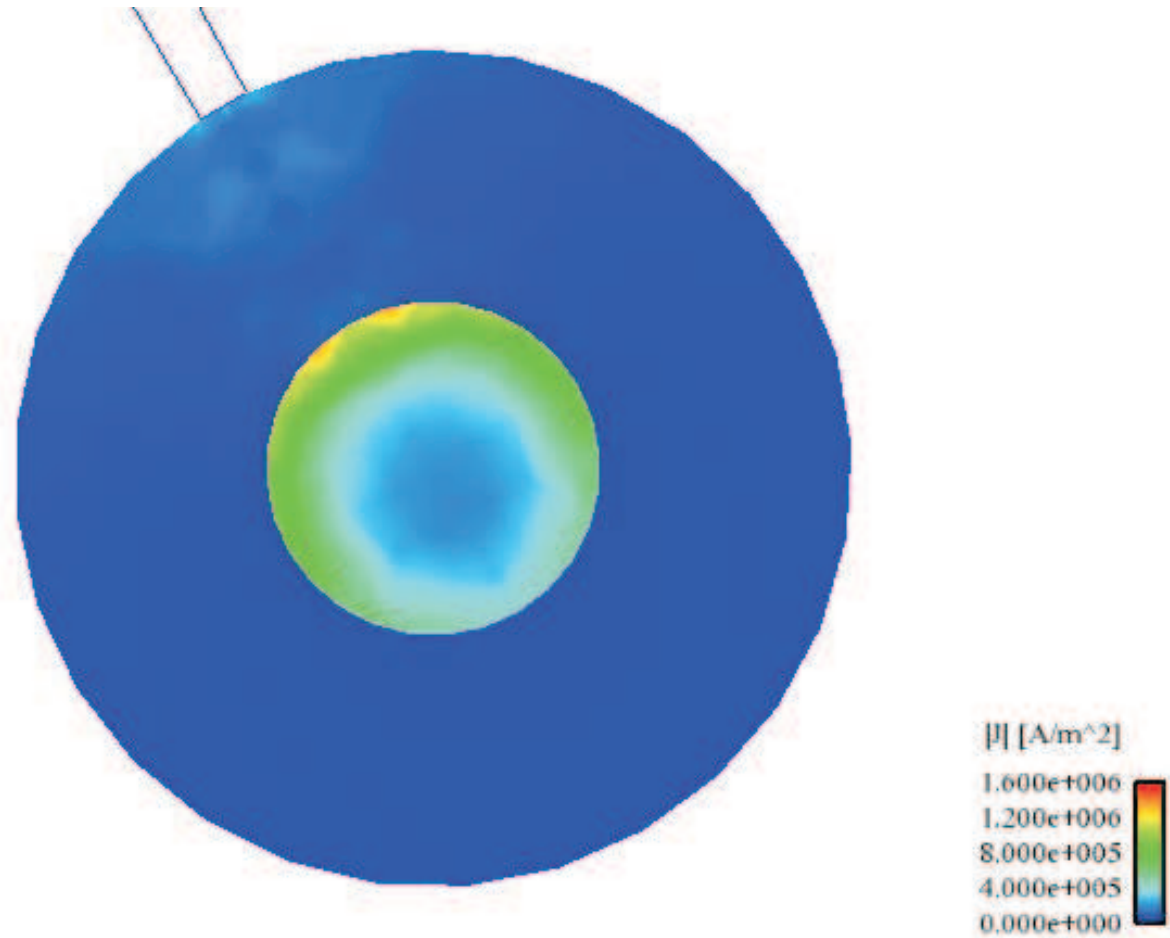
Data: $\sigma = 10^6 \Omega^{-1}\text{m}^{-1}$ for graphite, $\sigma = 10^4 \Omega^{-1}\text{m}^{-1}$ for Söderberg paste, $\sigma = 5 \times 10^6 \Omega^{-1}\text{m}^{-1}$ for copper, $\mu = 4\pi \times 10^{-7} \text{Hm}^{-1}$, $\omega = 50 \times 2\pi \text{ rad/s}$, $I_0 = 7 \times 10^4 \text{ A}$ for each electrode.

Numerical results for the Case C (cont'd)



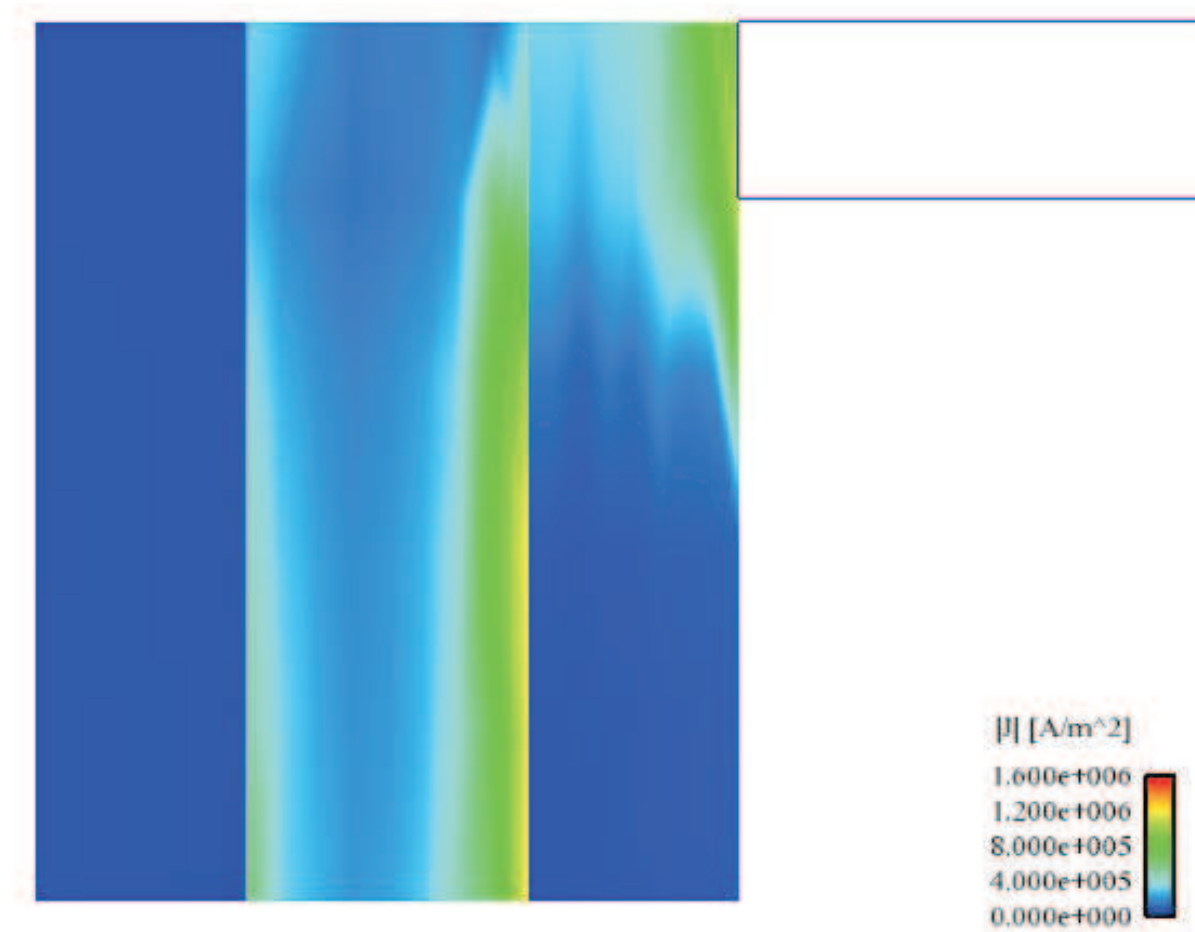
The value of the magnetic "potential" in the insulator: the magnetic field is the gradient of the represented function (not taking into account the jump surfaces).

Numerical results for the Case C (cont'd)



The magnitude of the current density $\mathbf{J}_{e,C} = \sigma \mathbf{E}_C$ on a horizontal section of one electrode.

Numerical results for the Case C (cont'd)



The magnitude of the current density $\mathbf{J}_{e,C} = \sigma \mathbf{E}_C$ on a vertical section of one electrode.

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